ROBERT B. FORREST *School of Surveying\* University of New South Wales Kensington, N.S.W., Australia* 

# Simulation of Orbital Image-Sensor Geometry

A Fortran program is presented, the parameters are listed, and the algorithms are described for the simulation of the Landsat MSS.

# **INTRODUCTION**

**A** FORTRAN computer simulation of orbital im-<br>age-sensor geometry is presented. The program models satellite, Earth-rotation and sensor dynamic behavior and provides the Earth-surface positions for any number of specified image locations. The user specifies the image-center latitude, longitude, and terrain height. In the form listed, the parameters used are those for the Landsat MSS. A few changes allow the coverage and distortions of other satellite orbits and image sensors to be analyzed. Thus, the program may be of use to those interested in studying the geometry

Widger (1966), Kratky (1971, 1974), Forrest (1974), and Puccinelli (1976) are incorporated. Readers unfamiliar with the Landsat orbit and the MSS sensor are referred to any of several related papers in this and other journals in the early 1970's.

# MSS COORDINATE SYSTEM

Input image locations are specified in rowcolumn pixel coordinates, *r* and *c.* As shown in Figure 1, *r* increases in the direction of Landsat motion, from north to south; and *c* increases in the direction of MSS scan sweep, from west to east. The simulation assigns integral row-column coordinate

ABSTRACT: *The essential dynamic aspects of orbital image-sensor geometry are modeled in a Fortran computer program presented and described in the paper.*  Parameters are listed for the Landsat *MSS, and the program is sufficiently versatile that it can be modified to simulate other image-sensor geometrics and formats. The program is organized to provide Earth-surface coordinate outputs (latitudellongitude, local Cartesian) for any number of image coordinate inputs (pixel rowlcolumn numbers). Individual terrain heights may be specified for each image point of interest.* 

and positional aspects of image data from future satellite imaging systems (spor, MOS, Landsat D). The form listed has been useful in showing the true ground coverage of a single MSS image, as well as the effects of varying satellite attitude on the coverage.

The program was written during an analysis of the geometric corrections applied to the electron beam recorder (EBR) used at the National Aeronautics and Space Administration Goddard Space Flight Center (NASA/GSFC) to produce Landsat MSS film images. To evaluate the adequacy of the EBR corrections, some theoretical values were needed. A modified form of the program described here provided those values. The simulation gives a precision of about one meter on the ground, more than adequate for any presently planned sat-

\* Through June, 1981.

PHOTOGRAMMETRIC ENGINEERING AND REMOTE SENSING, Vol. 47, No. 8, August 1981, pp. 1187-1193.

ellite imaging programs. Concepts discussed by values to pixel centers. Each pixel extends from  $-0.5$  to  $+0.5$  unit in each direction from its center. For one entire framed MSS image (or *scene* as it is regrettably called),  $0.5 \le r \le 2340.5$  and  $0.5 \le c \le$ 3240.5.

Most calculations for an image are referenced to the center. The simulation considers the image center pixel coordinates  $(r = 1170.5, c = 1620.5)$  to occur halfway between scan sweeps 195 and 196 of a framed Landsat image (Figure 1). This is a consequence of the even number of scan sweeps printed in a standard EBR framed MSS image. As Figure 2 shows, because there are six lines in each scan sweep, the image center normally is sensed slightly *before* the satellite passes over it. The satellite nadir at the moment the image center is sensed will vary, depending on the parameters applied in the simulation.

S  $\overline{l}$  $\overline{p}$ 

 $\eta$ 

 $\psi$ 



FIG. 1. Pixel coordinate system and details.

Figure **2** shows an ideal situation for two consecutive scan sweeps. Satellite attitude/altitude variations, MSS detector placement, and sweepcycle time all act to modify the ideal geometry. Ground details at or near the fore or aft edges of a scan sweep may be imaged twice, once, or not at all.



**FIG. 2.** Relation of satellite to scene center.

The following sensor- and format-related parameters are defined within the computer program. The values in brackets are those shown in the program listing for the Landsat MSS.

- $t_{sw}$  = Time for a complete scanner sweep cycle, seconds **(1113.62).**
- $\dot{p}$  = Active scan sweep-rate, pixels/ second **(100417.5).**
- $Q_{\alpha}Q_{\beta}Q_{\beta}Q_{\beta}$  = Coefficients of the sweep-rate nonlinearity correction in pixel column units, modeled as a cubic polynomial of sensed pixel column coordinate **(0,**   $-0.01733$ , 1.6043  $\times$  10<sup>-5</sup>,  $-3.3011 \times 10^{-9}$ .
	- = Scan sweeps per image **(390).**
	- $=$  Lines per scan sweep  $(6)$ .
	- = Total number of pixels in direction of scan for a single scan line **(3240).**
	- = Maximum angular coverage in
	- direction of scan, radians **(0.2).** = Angular coverage of a single scan sweep normal to the direction of scan, radians **(0.000514).**

# **EARTH ORBIT GEOMETRY**

Figure **3** shows the orbit geometry at imagecenter time,  $t_0$ . In the figure, a sphere of radius equal to that of the satellite's assumed circular orbit is centered on the reference Earth ellipsoid, also assumed to be the center of mass for the Earth. Earth-centered coordinates  $X, Y, Z$  have plus *X* passing through the equator at **0** degrees Iongitude, and plus **Z** through the North Pole. Time is measured from the ascending node, the point at which an individual orbit customarily is considered to begin. Angle **y** represents longitude of the descending node at time **to;** the fixed Landsat WRS orbital paths are not used. The spherical angle, **i,** is orbital inclination, about **99** degrees for Landsat's retrograde orbit. The azimuth of the orbital velocity vector at  $t_0$  is  $\alpha_0 = \beta_0 + \pi$ , and geocentric latitude is  $\Phi_0$ <sup>'</sup>.

The relationships between ellipsoidal and spherical parameters are shown in Figure 4, a meridional section at  $t_0$ . Altitude,  $H$ , is measured normal to the ellipsoid. The satellite velocity vector is normal to the radius of orbit, which in general is not parallel to the geodetic vertical.

The following orbital and ellipsoidal parameters are defined within the computer program, with the values used for the listing given in brackets:

- $a =$  Semimajor axis of the reference Earth ellipsoid, in metres **(6,378,165).**
- $e^2$  = Square of ellipsoid eccentricity
- $(i.0066935113)$ .<br> $i = \text{Orbital inclination of satellite, radians}$ **(1.72787596).**



FIG. 3. Orbital geocentric sphere.

- $R =$ Radius of orbit, metres  $(7,285,600)$ ; the program can be used for slightly elliptical orbits, taking the effective geocentric distance at image center as R.
- $\omega_s$  = Satellite angular velocity, radians per second (0.0010152871).
- $\omega_e$  = Earth angular velocity, radians per second, including orbit precession effects  $(7.2722052 \times 10^{-5})$ .

# PROGRAM DESCRIPTION

The program as listed (Figure 5) was written for a minicomputer (Digital Equipment Corp. PDP 11/40) which requires the use of double precision throughout to obtain the desired significance. The program has been organized for ease of understanding, rather than efficient execution.



FIG. 4. Geocentric and geodetic reference.

INPUTS

For each exercise of the program, the user provides a data file which includes:

- (1) Geodetic latitude and longitude of the image center,  $\Phi_0$  and  $\lambda_0$ , in decimal degrees.
- (2) Image-center terrain height above sea level in metres,  $h_{\theta}$ .
- (3) Sensor attitude angles  $\omega_0$ ,  $\phi_0$ ,  $\kappa_0$  at the time image center is sensed, in decimal degrees. Zero values correspond to alignment of the sensor coordinate axes **(x,y,z** in Figure 6) with the local vertical and satellite heading. (For those unfamiliar with this photogrammetric expression for attitude, the sensor tilt angles are Eulerian, defined in the order  $\omega$ —identical to roll, then  $\phi$ —analogous to pitch, and finally  $\kappa$ —analogous to yaw. The standard sign convention for positive  $\omega$ ,  $\phi$ , and  $\kappa$  corresponds to aircraft left wing up, nose down, and nose left, respectively).
- (4) Linear attitude changes with time,  $\dot{\omega}$ ,  $\dot{\phi}$ ,  $\dot{\kappa}$ , in decimal degrees per second.
- (5) A flag which shows whether the imagecenter terrain height is to be used for each image point processed (flag  $= 0$ ), or whether heights will be provided for each separate pixel considered (flag  $= 1$ ).
- (6) A list of image coordinates for which Earthsurface locations are desired, as pixel values  $r$  and  $c$  (Figure 1). If the flag in (5) above is set, terrain heights above sea level in metres also must be included for each image point.

### OUTPUTS

The program copies the input image-center information on the output data file. Then, for each image point specified, the program provides:

# **PHOTOGRAMMETRIC ENGINEERING** & **REMOTE SENSING, 1981**

RCLL-FEARTH-SURFACE COURDE: FROM PIETRIC STRINGLY TO CREAP CREAP (1991)<br>THPLICIT REALBOIG-HIJ: CO-2 (1991)<br>COMMON AIJE2, XINC.R.NS-NE-TPERSM.PDOT.<br>HOO.OI.O2.03.5 SMIM-PPL.PETA-PPERSM.PDOT.<br>HOO.OI.O2.03.5 SMIM-PPL.PETA-PSI. CALL SETFIL(1,'MSS1.DAT',IERR;'DKI',O)<br>CALL SETFIL(2,'MSS2.DAT',IERR;'DKI',O)<br>DTOR=.0174532925 HALFPI=90.#DTOR<br>C#####IMAGE SENSOR/FORMAT PARAMETERS<br>TPERSW=1./13.62<br>SWIM=390.  $PPL = 3240.$ ETA=0.2<br>PSI=.000514<br>PDOT=100417.54 01--0.01733 02-1.60430-05 03=-3.3011D-09<br>C#####EARTH ELLIPSOID AND EFFECTIVE EARTH ANG. VELOCITY WE=7.2722052D-05<br>C#####CIRCULAR ORBIT VALUES: RADIUS, INCL., ANG. VELOCITY CRIENTING GREEN CRIP (1997-1017 FOR THE PAPEL IS A REVENUES ARE CRIP (1997-1017 FOR THE PAPEL IS A REVENUES IN THE TANK OF TH .S=XLS+XLZ-XL LOCESS EACH PIXEL IN FILE 201 FORMAT(\* 1801)<br>1976 - Anton Caroline, Fransız Amerika, Azar Your (\* 1717)<br>2 IF(1814, EQ.0) 80 TO 5<br>2 IF(1814, EQ.0) 80 TO 5<br>6 READ (17204, ERPB=99) ROW-COL-HH<br>50 TO 6<br>204 FORMAT(2F7, 11-F6.0)<br>6 CALL MSSR(ROW-COL-172, G 99 END SUBROUTINE **MSSA(PHZ~XLZITZ.OAMMA~BETAIH)** C###LAT/LONG OF IMAGE CENTER IN‡ TIME OF IMAGING;<br>C DESC. NODE, AND (AZIMUTH-IBO DEGREES) OUT.<br> IMPLICIT DOUBLE PRECISION (A-H),(O-Z) COMMON AIRED AT A CONTRACT AND MATERIAL CONTRACT AND A CONTRACT AND RESERVATION ON A CONTRACT AND A CONTRACT AND A CONTRACT AND A CONTRACT OF A CONTRACT

FOR SURGIOUTRE MSSE(ROW-COL-7T-GAMMA OEZ-DOEFFH-XL, XE,<br>
IMPLICIT DOUBLE PRECISION (A-M) (C)<br>
IMPLICIT DOUBLE PRECISION (A-M) (C)<br>
IMPLICIT DOUBLE PRESSLAP (PRESSLAPDIT)<br>
100MNA AI.EZ-XINC, R.W.S.NE, TPENSALPDIT<br>
100MNA AI PHS=PHP<br>
PAS-PHP<br>
DO 2 I=1+3<br>
XM=AI/DSGRT(11-E2#DSIN(PHS)\*DSIN(PHS)\*<br>
SP=XM#E2#DSIN(PHS)\*DCDS(PHS)/R<br>
SP=XM#E2#DSIN(PHS)\*DSGRT(11-SP#SP))<br>
C#### SATELLITE ALTITUDE+LONGTIDE-MEADING<br>
DL=-DATAN2(DSIN(RHO)+DCDS(RHO)\*CI)<br>
XLS= C###ROTATION FROM EARTH TO LOCAL-VERTICAL COORDS<br>C###IMAGE/SATELLITE FR≀MHS,XLS)<br>C###IMAGE/SATELLITE FROM LOCAL-VERTICAL TO EARTH COORDS. DO 4 J-1,3<br>
A XPP(I)\*R(1)+B(J,I)\*XP(J)<br>
C\*\*\*SCALE IMAGE VECTOR TO TERRAIN HT, ABOVE ELLIPSOID<br>
V2=(A1+HH)\*K(A1+HH)\*1,D-12<br>
UL-DESORT(A1+HH)\*1,D-12<br>
US-ULWIUM1,D-12<br>
XS(3)=XS(3)-DSIN(PHS)\*XXWEC<br>
AK-U2\*(XPP(1)\*XP(1)+XPP(2)\*X SUBROUTINE ROTAT(A+OE)<br>
C#### 3-DIMENSIONAL ROTATION MATRIX \*A\*<br>
IMPLICIT REAL#B(A-H)+(O-Z)<br>
DIMENSION A(3+3)+OE(3)<br>
SW-DSIN(OE(1))<br>
CW-DCOS(OE(1)) SP=DSIN(DE(2))<br>CP=DCOS(DE(2))<br>SK=DSIN(DE(3))  $\begin{array}{ll} \texttt{SK-DSIN}(\texttt{OC(3)})\\ \texttt{CK-DSIN}(\texttt{OC(3)})\\ \texttt{A(1,1)}=\texttt{CPKCK}\\ \texttt{A(2,1)}=\texttt{CPKCK}\\ \texttt{A(3,1)}=\texttt{SP}\\ \texttt{A(3,1)}=\texttt{SP}\\ \texttt{A(3,2)}=\texttt{-SWKCP}\\ \texttt{A(3,2)}=\texttt{GU*CF}\\ \texttt{A(3,2)}=\texttt{CU*CKF}+\texttt{A1*CK}\\ \texttt{A(2,2)}=\texttt{CU*CKF}-\texttt{A1*SK}\\ \texttt{A(2,2)}=\texttt{$  $AI = C W R S P$ A(2,3)=SW\*CK+A1\*SM<br>RETURN END IMPLICIT DOUBLE PRECISION<br>DIMENSION A(3,3)<br>SX=DSIN(X) CX=DCOS(X> SY=DSIN(Y)<br>CY=DCOS(Y) SZ=DSIN(2)<br>CZ=DCOS(2)<br>A(1+1)=SX\*SZ+CX\*SY\*CZ<br>A(1+2)=-SX\*CZ+CX\*SY\*SZ<br>A(2+2)=CX\*CZ+SX\*SY\*CZ<br>A(2+2)=CX\*CZ+SX\*SY\*SZ A(2,3)=-SX\*C<br>A(3,1)=CY\*CZ A(3,2)=CY\*S<br>A(3,3)=SY<br>RETURN END

**FIG. 5. Fortran program listing.** 

1190



- (1) Geodetic latitude and longitude in decimal degrees, and
- (2) Local Cartesian coordinates  $\hat{X}$ ,  $\hat{Y}$ , and  $\hat{Z}$  in and then metres. Within the reference plane, the  $\hat{X}$ ,  $\hat{Y}$ ,  $\hat{Z}$  origin is at image center, with positive  $\hat{X}$  in the direction of satellite heading and  $\hat{Z}$

### LIMITATIONS

An optical-mechanical west-to-east scanning sensor is modeled in the program as listed. With a few changes a fixed linear array can be simulated. The internal mss imaging geometry is not modeled in great detail, except for mirror sweep rate. MSS detector offsets or placement errors are not included, nor are the so-called commutation effects caused by the sampling sequence. Such effects generally are seen as simple image-space pixel translations. The listed program assumes a circular or near-circular orbit, as stated earlier. It is not subsequently suitable for orbit inclination of exactly zero, or for images centered on the night side of an orbit. This routine calculates latitude,  $\Phi$ , and lon-

Long), first reads the image center data from the turned. The image-center values for  $t_0$  and  $\gamma$  are Long), first reads the image center data from the  $\frac{1}{2}$  regiments are all as parameters for allineard set Long), its reads the mage center tast from  $X, Y, Z$  to<br>  $\hat{X}, \hat{Y}, \hat{Z}$ . Next, subroutines MSSA and MSSB are called<br>
iteratively to obtain the fundamental image-center<br>
quantities  $t_0, \gamma$ , and  $\beta_0$  (Figure 3). RCLL th quantities  $t_0, \gamma$ , and  $\beta_0$  (Figure 3). RCLL then reads and processes each input image point in turn. Sub-  $(2)$  Attitude angles  $\omega$ ,  $\phi$ , and  $\kappa$  for the satellite at routine MSSB returns the latitude,  $\Phi$ , and longitude,  $t$ ;

 $\lambda$ , for the specified pixel coordinates and terrain<br>elevation, and also provides the X, Y, Z coordinates.<br>RCLL develops  $\hat{X}, \hat{Y}, \hat{Z}$  and writes the final ground<br>coordinate values to the output data file. elevation, and also provides the **X,Y,Z** coordinates. RCLL develops  $X, Y, Z$  and writes the final ground coordinate values to the output data file.

# **ANALYSIS**

# SUBROUTINE MSSA

From the given image-center coordinates,  $\Phi_0$ and  $\lambda_0$ , this routine develops three fundamental orbit-related quantities:

- $t_0$ , the time in seconds at which  $\Phi_0$  and  $\lambda_0$  were actually sensed,
- $\gamma$ , longitude of the descending node at  $t_0$ , and  $\alpha_0$ , azimuth of the orbital path at  $t_0$ .

First, the geocentric latitude,  $\Phi_0'$ , is found which corresponds to  $\Phi_0$ : i.e.,

$$
\Phi_0' = \Phi_0 - \sin^{-1}(Ne^2 \sin \Phi_0 \cos \Phi_0 / R)
$$

where

$$
N = a/(1 - e^2 \sin^2 \Phi_0)^{1/2}.
$$

Then, satellite altitude above the ellipsoid is

$$
H = R \cos \Phi_0 / \cos \Phi_0 - N.
$$

FIG. 6. Sensor coordinate system. Next, the orbital arc distance,  $\rho_0$ , from the antinode (Figure 2) is found:

$$
\rho_0 = \cos^{-1}(\sin \Phi_0'/\sin i)
$$

$$
t_0 = (\rho_0 + \pi/2)/\omega_s - t_{sw}/2, \qquad (1)
$$

E origin is at mage center, which positive  $\hat{Z}$  may be calculated directly. The  $t_{sw}/2$  term results from the definition of  $t_0$  as the time image center is positive upward. Sensed, not the time the satellite is passi image center (Figure 2).

> Continuing, the longitude difference at  $t_0$  between image center and the anti-node is<br>  $\Delta \lambda = \pi - \tan^{-1}(\tan \rho_0/\cos i),$

$$
\Delta\lambda = \pi - \tan^{-1}(\tan \rho_0/\cos i),
$$

so that

$$
\gamma = \lambda_0 - \pi/2 + \Delta\lambda. \tag{2}
$$

Finally, the orbital azimuth at  $t_0$  is  $\alpha_0 = \beta_0 + \pi$ , where

$$
\beta_0 = -\tan^{-1}(\cot i/\sin \rho_0). \tag{3}
$$

gitude,  $\lambda$ , of a point on the Earth at specified pixel ORGANIZATION coordinates, *r* and c, and terrain height, h. Earth-The main program, RCLL (Row/Column to Lat) centered coordinates  $X, Y, Z$  (Figure 1) also are re-

- 
- 
- (3) Satellite latitude, longitude, and altitude  $\Phi_s$ ,  $\lambda_{s}$ , and H at t;
- (4) Image-sensor coordinates  $x,y,z$  rotated to a local vertical reference;
- (5) Rotation from local-vertical to Earth-centered coordinates; and
- (6) Calculation of @, **A.**

Each of these is briefly discussed below.

Time. The program uses a "continuous pixel" in the direction of scan sweep: if  $c = 1816.3$ , the time is found which corresponds exactly to 1816.3 pixel-times from start of scan sweep. This convention is admittedly somewhat artificial, since pixel sampling only takes place at integral pixel times, 1816.0 in this example. If the distinction is important, input c values should be limited to integer values.

The sweep number relative to the first scan sweep in the image is

$$
n = [r + |r|(l - 0.501)/r]/l.
$$

Sweep-rate nonlinearity is removed next:

$$
c' = c + Q_0 + Q_1c + Q_2c^2 + Q_3c^3,
$$

where  $c'$  is the equivalent constant-sweep-rate column coordinate.

Then

$$
t = t_0 + t_{sw}(n - s/2) + (c' - p/2 - 0.5)/p
$$

where the three terms represent time for image center, time for whole scan sweeps, and time within sweep *n*.

Attitude. Satellite attitude at t is calculated using  $\omega_0$ ,  $\phi_0$ ,  $\kappa_0$  and  $\dot{\omega}$ ,  $\dot{\phi}$ ,  $\dot{\kappa}$ . Subroutine **ROTAT** returns a three-dimensional rotation matrix, A, which indicates the alignment of the image sensor Cartesian coordinates  $x,y,z$  with respect to the local vertical and satellite heading.

Satellite Location. Geocentric satellite latitude at t is

$$
\Phi'_{s} = \sin^{-1}(\cos \rho_{s} \sin i),
$$

where

 $\rho_s$  = orbital arc distance from anti-node<br>=  $\omega_s t - \pi/2$ .

An iterative technique is used to develop geodetic latitude of the satellite,  $\Phi_{s}$ . Initial approximation  $\Phi_1 = \Phi'_s$  is entered in

$$
\tilde{\Phi}_{i+1} = \Phi'_{s} + \sin^{-1}(N_{i}e^{2} \sin \tilde{\Phi}_{i} \cos \tilde{\Phi}_{i}/R),
$$

with

$$
N_i = a/(1 - e^2 \sin^2 \tilde{\Phi}_i)^{1/2},
$$

and the determination repeated twice, with  $\Phi_3$ taken as  $\Phi_s$ . Then satellite altitude is<br>  $H = R \cos \Phi_s'/\cos \Phi_s - N$ .

$$
H = R \cos \Phi_{s} / \cos \Phi_{s} - N.
$$

Satellite longitude at t is

$$
\lambda_s = \gamma - \pi/2 + \tan^{-1}(\tan \rho_s/\cos i) - \omega_e(t - t_0),
$$

in which the last term adjusts for Earth rotation between times  $t$  and  $t_0$ . Finally, orbital heading,  $\beta_s$ , at t is found using the same form as Equation 3.

Sensor Coordinate Vector. The simulation converts pixel coordinates  $r,c'$  to right-hand Cartesian coordinates x,y,z (Figure 6). The **x** axis coincides with the scan sweep axis, positive in the forward satellite direction. The *z* axis coincides with the scanner's optical axis at sweep center and is positive upward. Using the scanner's field-of-view parameters  $\psi$  and  $\eta$ ,

$$
x = \psi(r - nl + l/2 - 0.5)/l,
$$
  
\n
$$
y = \sin \theta, \text{ and}
$$
  
\n
$$
z = -\cos \theta,
$$

where

$$
\theta = \eta(c' - p/2 - 0.5)/p.
$$

The sensor-coordinate vector  $(x,y,z)$  then is transformed to a satellite-vertical unit vector by

$$
\begin{bmatrix} x' \\ y' \\ z' \end{bmatrix} = A^{\mathrm{T}} \frac{1}{(1+x^2)^{1/2}} \begin{bmatrix} x \\ y \\ z \end{bmatrix}
$$

Ground Coordinate Rotation. The values for  $\Phi_{s}$ ,  $\lambda_s$ , and  $\beta_s$  at t can be used to define the orientation of the local vertical vector  $(x',y',z')$  to the Earthcentered **X,Y,Z** coordinates. Subroutine **ROT^** returns the rotation matrix, B, from which

$$
\begin{bmatrix} x'' \\ y'' \\ z'' \end{bmatrix} = \mathbf{B}^{\mathrm{T}} \begin{bmatrix} x' \\ y' \\ z' \end{bmatrix}
$$

Location of the Point. Satellite coordinates at t can be defined as  $(0,0, N + H)$  in a local-vertical coordinate system aligned with the  $x', y', z'$  axes, but with origin at the curvature center of the prime vertical, N, in Figure 4. After rotation through  $B<sup>T</sup>$ and an offset in Z, the Earth-centered coordinates of the satellite at t are

$$
X_s = b_{31}(N + H),
$$
  
\n
$$
Y_s = b_{32}(N + H),
$$
 and  
\n
$$
Z_s = b_{33}(N + H) - Ne^2 \sin \Phi_s.
$$

To find the place where the extended  $(x'', y'', z'')$ vector pierces the ellipsoid at terrain height  $h$ , a modified version of Puccinelli's (1976) method is used. A parametric form for the vector from ellipsoid center to the desired point would be

$$
\begin{bmatrix} X \\ Y \\ Z \end{bmatrix} = (a + h) \begin{bmatrix} \cos \lambda & \cos \phi \\ \sin \lambda & \cos \phi \\ \sin \phi \end{bmatrix}
$$
 (4)

where  $\Phi$  is not in general equal to  $\Phi$ . A second form is

$$
\begin{bmatrix} X \\ Y \\ Z \end{bmatrix} = \begin{bmatrix} X \\ Y \\ Z \end{bmatrix}_s + U \begin{bmatrix} x'' \\ y'' \\ z'' \end{bmatrix}
$$
 (5)

where *U* is an unknown scale factor which must be

1192

equations are obtained in  $\lambda$ ,  $\hat{\Phi}$ , and *U*. Eliminating the two angles, a quadratic in *U* is obtained:

$$
U^2u^2[(x''^2 + y''^2) + v^2z''^2] + 2U[u^2(X_sx'' + Y_s y'')+ v^2Z_sz'']+ u^2(X_s^2 + Y_s^2)+ v^2(Z_s^2 - u^2) = 0,
$$

$$
u = a(1 - e^{2})^{1/2} + h
$$
, and  
\n
$$
v = a + h.
$$

The quadratic is solved for the smaller root, and Survey and Mr. G. J. Grebowsky of NASA/GSFC<br>the final Earth-centered coordinates are found provided valuable information, cooperation, and the final Earth-centered coordinates are found provided valuable information, cooperation, and using Equation 5. Finally, latitude and longitude stimulating discussions in connection with the using Equation 5. Finally, latitude and longitude stimulating discussions in connection with the

$$
S = (X2 + Y2)1/2,\n\Phi = \tan-1[(Z/S) (a + h)/(a(1 - e2) + h)],\n\lambda = \tan-1 (Y/X)
$$

The program has proven to be of benefit in es-<br>tablishing the actual shape on the Earth for a tablishing the actual shape on the Earth for a<br>single MSS Images. Proceedings, International Society of<br>not always obvious. For example, Landsat head-<br>photogrammetry Commission III Symposium, ing is due west at the anti-node and about nine<br>degrees west of south at the equator. Thus, one Kratky V 1971 Precision Processing of ERTS Imag degrees west of south at the equator. Thus, one Kratky, V., 1971. Precision Processing of ERTS Imagery.<br>might expect the ground coverage for a single *Proceedings of the American Society of Photo-*<br>northern-hemisphere scen northern-hemisphere scene to be slightly compressed on the east side and expanded on the west single mss scene. The details of a typical shape are<br>
not always obvious. For example, Landsat head-<br>
ing is due west at the anti-node and about nine<br>
degrees west of south at the equator. Thus, one<br>
might expect the groun side from its nominal dimensions. The simulation grammetric Engineering, **40:2,** pp. **203-212.**  shows that the reverse effect takes place, as the Puccinelli, E. F., 1976. Ground Location of Satellite Earth rotation and orbit inclination effects over-<br>Scanner Data. Photogrammetric Engineering and Earth rotation and orbit inclination effects override the azimuth change effect. Remote Sensing, **42:4,** pp. **537-543.** 

image-sensor with the same orbit and image for-<br>mat as Landsat, make the following parameter ellite Observations of the Earth and its Atmosphere. mat as Landsat, make the following parameter ellite Observations of the Earth and its Atmosphere.<br>
changes:  $t = 1/81.72$ ,  $s = 2340$ ,  $l = 1$ ,  $u = 8.57$ , *Proceedings, Fourth Remote Sensing Symposium,* changes:  $t_{sw} = 1/81.72$ ,  $s = 2340$ ,  $l = 1$ ,  $\psi = 8.57 \times$  Proceedings, Fourth Remote Sensing Symposium,<br>10<sup>-5</sup>  $\dot{s} = 10^{29}$  and  $\dot{O} = 0 = 0$ ,  $\dot{O} = 0$ ,  $\dot{$ 

Of course, the program as listed addresses only half the general positioning problem. Often of (Received 28 June 1979; revised and accepted 9 De-<br>more interest is the inverse transformation, i.e., cember 1980)

applied to the unit vector  $(x'', y'', z)$ . By equating the calculating the image location which corresponds two sets of expressions (Equations 4 and 5), three to a given Earth-surface position. Because of the equations are obta to a given Earth-surface position. Because of the proven convenient to solve such problems iteratively, using a modified portion of program RCLL as<br>a subprogram. Some arbitrary pixel coordinates are used as initial estimates, and the resulting<br>Earth-surface positions calculated by r.c.L. are where used to improve the estimates.

 $v = a + h$ .<br>The quadratic is solved for the smaller root, and Survey and Mr. G. I. Grebowsky of NASA/GSFC work described here. My thanks also to the anonymous reviewer who suggested simplified forms for two of the equations. Much of the work described here was performed during a temporary research appointment with the EROS Program Coordinator, Topographic Division, U.S. Geologi-COMMENTS cal Survey, Reston, Virginia.

- 
- 
- 
- 
- To see the ground coverage of a linear array Widger, W. K., Jr., **1966.** Orbits, Altitudes, Viewing Ge- $10^{-5}$ ,  $\dot{p} = 10^{20}$ , and  $Q_0 = Q_1 = Q_2 = Q_3 = 0$ . University of Michigan Institute of Technology, Ann Arbor, pp. 489-537.

# **Bibliography Available**

The Bibliography of Remote Sensing in Forestry 1950-1978 has recently been completed by its authors, Brian J. Myers and Ian E. Craig. Its purpose is to provide ready reference to the voluminous literature documenting the use of remote sensing in forestry. The authors do not claim to have included all possible articles on the subject, but do hope that it is reasonably comprehensive within its terms of reference. The sources from which these articles have been drawn were restricted to material which would normally be readily available to the user through a forestry library. The sources include most English language forestry, photogrammetric, and remote sensing journals and the proceedings of regular relevant symposia, but not monographs, foreign language journals, or reports and publications of limited circulation.

Copies of the Bibliography may be obtained free of charge from

Mr. Brian J. Myers Division of Forest Research CSIRO P.O. Box 4008 Canberra, A.C.T. 2600 Australia